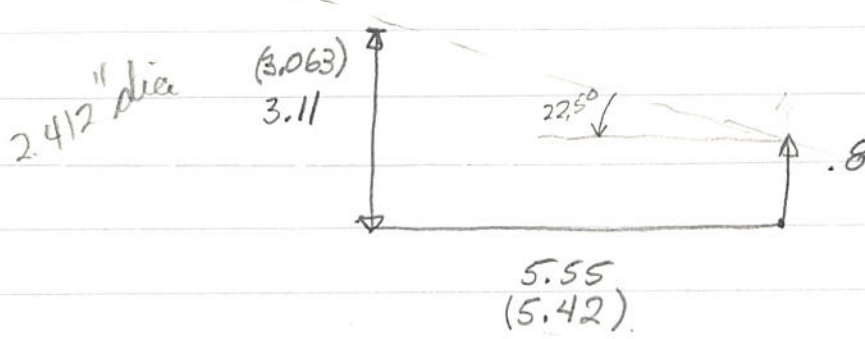


Summary of Changes in Calibrator Readings
 shown in the difference from measured disintegration
 values taken at ETR on August 28 for 1-10 unit.

	<u>Aug 28 @ Room</u>	<u>Oct 30 @ 0.3°C</u>	<u>D, %</u>	<u>Thermal Shift +25°C @ -air</u>
A1	210 KeV	212 KeV	-1%	1.3%
A2	440	455	-3%	1.5%
A3	925	946	+2%	1.8%
A4	2.38 MeV	231	-2.9%	2.0%
A5	4.45	4.59	+2.4%	2.5%
A6	9.48	8.75	-7.7%	0.8%
A7	21.2	20.9	-1.6%	0.9%
B1	206 KeV	197	-4.3%	4.1%
B2	445	401	-10%	3.5%
B3	809	861	+6.7%	3.5%
B4	3.82 MeV	3.88	+1.5%	0.9%
B5	7.51	7.31	-2.7%	-2%
B6	14.8	15.4	+4.1%	4.2%
C2	2.98	3.01	+1.1%	.3%
C3	3.95	3.97	+0.5%	.7%

1.3
+ 1.2
1.50 "

4 $\sqrt{22}$ 5.5



$$G = \frac{\pi}{2} \left\{ \underbrace{R_1^2 + R_2^2 + l^2}_{41.1146} - \left[\underbrace{(R_1^2 + R_2^2 + l^2)^2 - 4R_1^2 R_2^2}_{41.1146} \right]^{1/2} \right\}$$

(39.398)

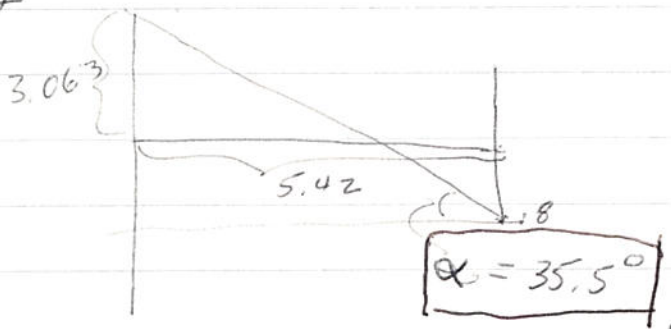
.3058

$$G = 1.51 \text{ cm}^2 \text{ sr.}$$

$$G = 0.320 \text{ cm}^2 \text{ sr.}$$

$$P7 = \text{flux} * G(7)$$

MAX 4

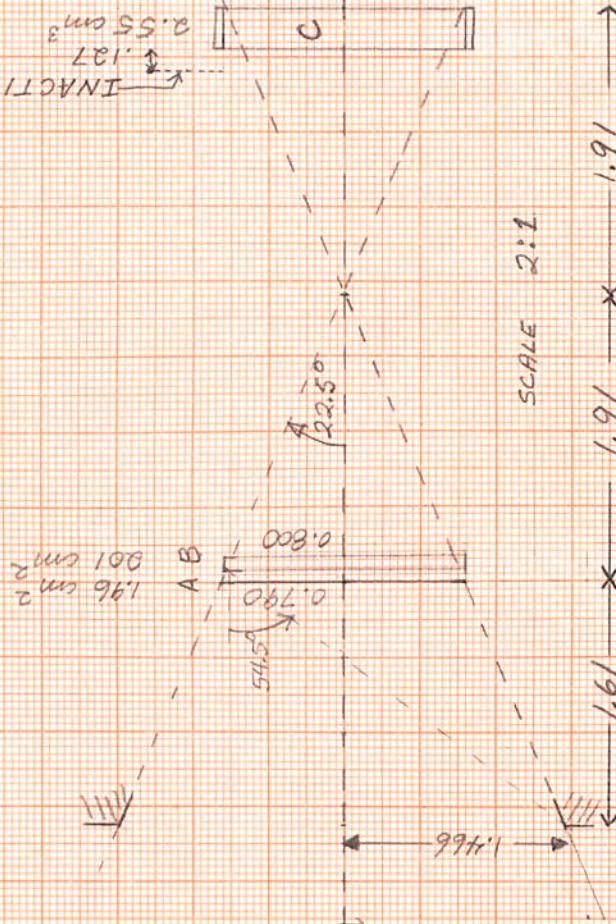
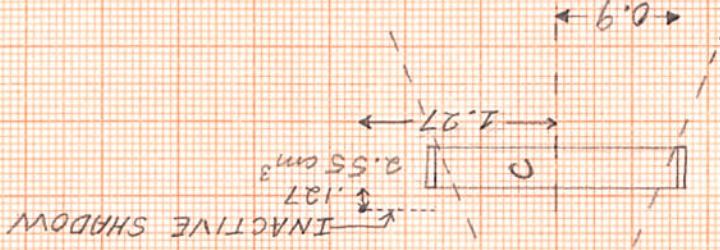


proj depth factor = 1.23 μ
= 50.96 for J

9/6/72

$$G = \frac{\pi^2}{2} \left\{ R_1^2 + R_2^2 + l^2 - \left[R_1^2 + R_2^2 + l^2 \right]^{\frac{1}{2}} - 4R_1 R_2 \right\}^{\frac{1}{2}}$$

(p. 42 NASA SP 243, GLOECKLER)

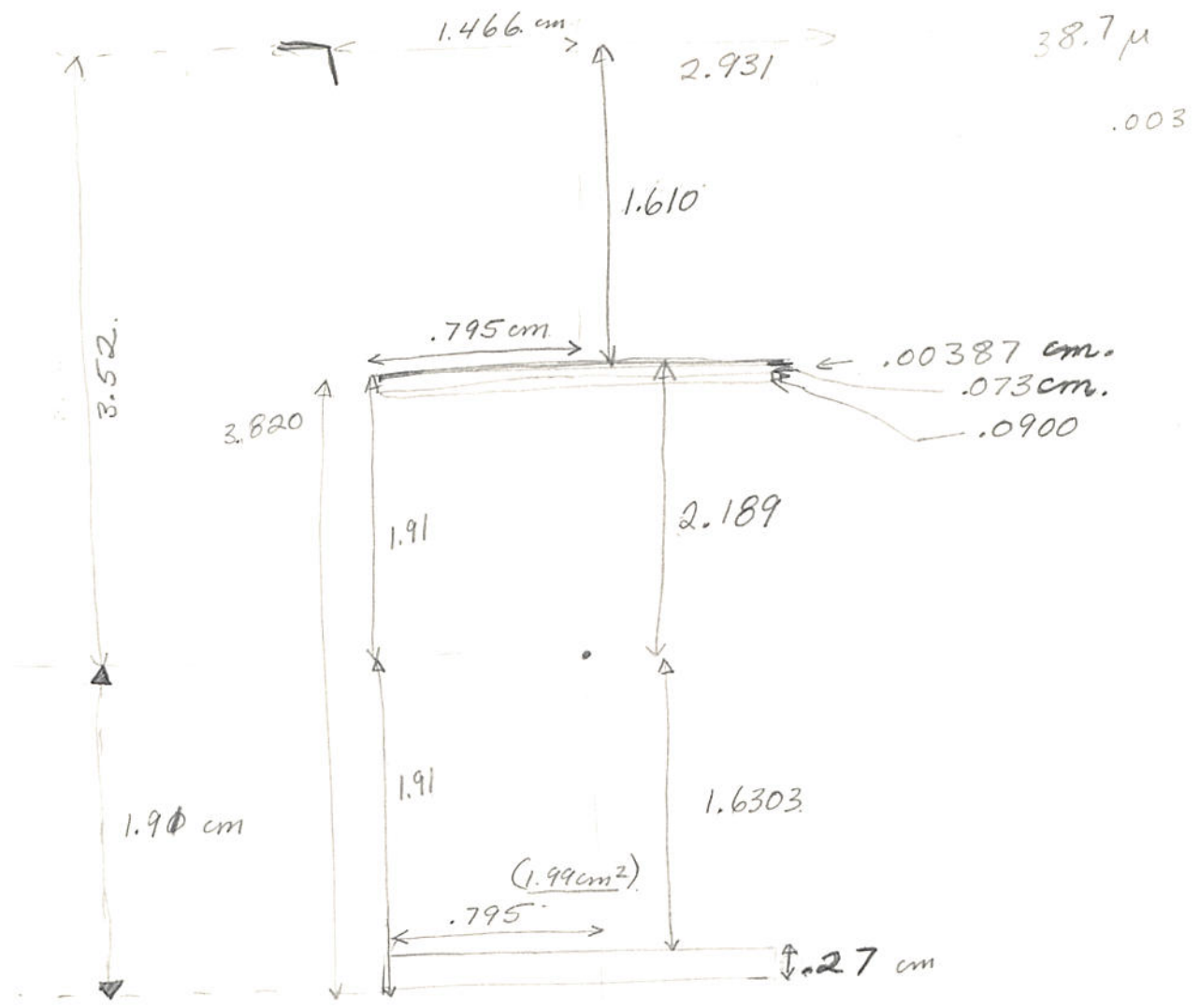


SCALE 2:1

CASES	R_1	R_2	l	G
A, B, AB	1.466	.8	1.61	2.66 cm ² sr (wrong)
BC	.8	.9	3.82	0.320 cm ² sr
\overline{BC}	.8	1.27	3.42	0.734 cm ² sr (0.414 cm ² sr)

1.79 MEV A point
 18 MEV B point

(15,8724



5.38125

13.9493
13.8005

August 28, 1972
 G. J. Kennedy
 Inst. C2 Repair

Thresholds

Calibrator

A1	210 KeV	A1.	1030
A2	440	A2.	375
A3	925	A3.	806
A4	238 MeV	A4.	1122
A5	4.48	A5.	111
A6	9.48	A6.	1437
A7	21.2 MeV	A7.	816
B1	206 KeV	B1.	915
B2	445	B2.	1190
B3	809 KeV	B3.	589
B4	3.82 MeV	B4.	626
B5	7.51	B5.	200
B6	14.8	B6.	656
C1	1.49	C2.	915
C2	2.98	C3.	317
C3	3.95	C4.	151
C4	6.95		
C5	26.4		
B7 ⁺	180.1 MeV		
A0	170	M	
B0	196	S	
C0	323		

AP's

AP1	250 ⁽⁵⁾ , 25 ⁽²⁾
	2.81 ⁽⁵⁾ , 06 ⁽⁴⁾
	3-01
	4 120
	5 192
	6 (5) 439 (3) 152
	(4) 2913 or
	112 413 (6) 300
	7 (5) 1500 or
	8 (5) 147 (5) 448

Voltages

-23	- 256
+6	- 597
+20	- 206
+250	- 213
+450	- 257
HV1	- 368
HV2	- 331

Noises

A0	132	202
A3	898	150
B0	183	210
B3	795	822
C0	311.5	335

Logic

P1	✓
P2	✓
P3	✓
P4	✓
P5	✓
P6	✓
P7	✓
P8	✓
P9	✓
P10	✓
P11	✓
α1	✓
α2	✓
α3	✓
α4	✓
α5	✓
α6	✓
α7	✓
Z1	✓
Z2	✓
E4	✓
E5	✓
E6	✓

Calibrator

A1	183
A2	434
A3	929
A4	2251
A5	4501
A6	7790
B1	221
B2	432
B3	833
B4	3907
B5	8227
B6	15011
C2	3167
C3	4448

PET Foil Thickness - Imp Htd

3 July 72

J.C.

PET SN	Foil (Num) μ inches	Foil (Measured) μ inches	PKG
002	12.5	13.68	APP1-10
003	12.5	11.9	APP1-11

Tom:

measured thickness of
foil was 28 μ inches.

J.C.

Foil = 12×10^{-4} INCHES Ni
 = 30.5×10^{-6} cm = .0000305 cm =

2147-0117 2147/12

Final Discrimination level settings for
 IMP H Flight Unit

Detector A₀ = .164

Detector	Present Level (Hw)	Desired Level (Hw)
A1 } 62 KEV	.220	<u>.210</u>
A2 } 62 KEV	.437	<u>.437</u>
A3 } 62 KEV	.923	<u>.923</u>
A4) 80 KEV	2.58	2.50 ^{SHE} _{2.4}
(A ₀) A5) 80 KEV	4.63	4.50
A6 } 80 KEV	8.85	10.0 - 9.5
A7 } 80 KEV	22.3	<u>21.0</u>
Z	180.00	<u>180.00</u>

Detector B B₀

B1	.244	.209	<u>.200</u>
B2	.438	.456	<u>.460</u>
B3	.826	.826	<u>.826</u>
B4	3.60	3.90	<u>3.90</u>
B5	7.81	7.70	<u>7.70</u>
B6	14.0	15.0	<u>15.0</u>
B7	31.0	25.0	<u>25.0</u>

Detector C

C1	1.50	1.50	<u>1.50</u>
C2	3.02	3.00	<u>3.00</u>
C3	4.96	4.05	<u>4.0</u>
C4	7.88	7.30	<u>7.0</u>
C5	30.1	27.0	<u>26.0</u>

D1 = 38.7M (ORTEC.)
 D2 = 900M - meas at NRL ^{Actually}
 D3 = 2700M. " _{SREL measured}

latest for spr 72 Calib Σ mp H 1-light.
 Energy Range (Nominal)

P1	A1 $\overline{B1}$ $\overline{A2}$ \overline{M}	0.275 - 0.500
P2	A2 $\overline{A3}$ $\overline{B1}$ \overline{M}	0.500 - 0.970
P3	A3 $\overline{B1}$ \overline{M}	0.970 - 1.80
P4	A1 B1 $\overline{B4}$ $\overline{C1}$ \overline{M}	1.80 - 3.9
P5	A1 B4 $\overline{B5}$ $\overline{C1}$ \overline{M}	3.9 - 8.0
P6	B5 A1 \overline{M}	8.0 - 14.0
P7	C4 B4 $\overline{B5}$ \overline{M}	14 - 26
P8	C4 B3 $\overline{B4}$ \overline{M}	26 - 46
P9	C4 C3 $\overline{C4}$ B3 $\overline{B4}$ \overline{M}	
P10	C2 $\overline{C3}$ B3 \overline{M}	
P11	C1 $\overline{B3}$ $\overline{C2}$ $\overline{B0}$	
$\alpha 1$	A4 $\overline{A5}$ $\overline{B1}$ \overline{M}	2.6 - 4.6
$\alpha 2$	A5 $\overline{B1}$ \overline{M}	4.6 - 7.4
$\alpha 3$	A4 B1 $\overline{B6}$ \overline{M}	7.4 - 17
$\alpha 4$	B6 $\overline{B7}$ $\overline{C1}$ A0 \overline{M}	17 - 26 48
$\alpha 5$	B7 $\overline{C1}$ A2 \overline{M}	26 - 48
$\alpha 6$	C5 B6 \overline{M}	48 - 95
$\alpha 7$	C5 $\overline{B6}$ B4 \overline{M}	95 - 190
Z1	A6 $\overline{B1}$ \overline{M}	
Z2	A7 $\overline{B1}$ \overline{M}	
E4	B1 $\overline{A1}$ $\overline{B5}$ $\overline{C2}$ \overline{M}	
E5	B2 $\overline{A1}$ $\overline{B5}$ $\overline{C2}$ \overline{M}	
E6	B3 $\overline{A1}$ $\overline{B5}$ $\overline{C2}$ \overline{M}	
Z3	A8 \overline{M}	

(for memo)

51P x 3045

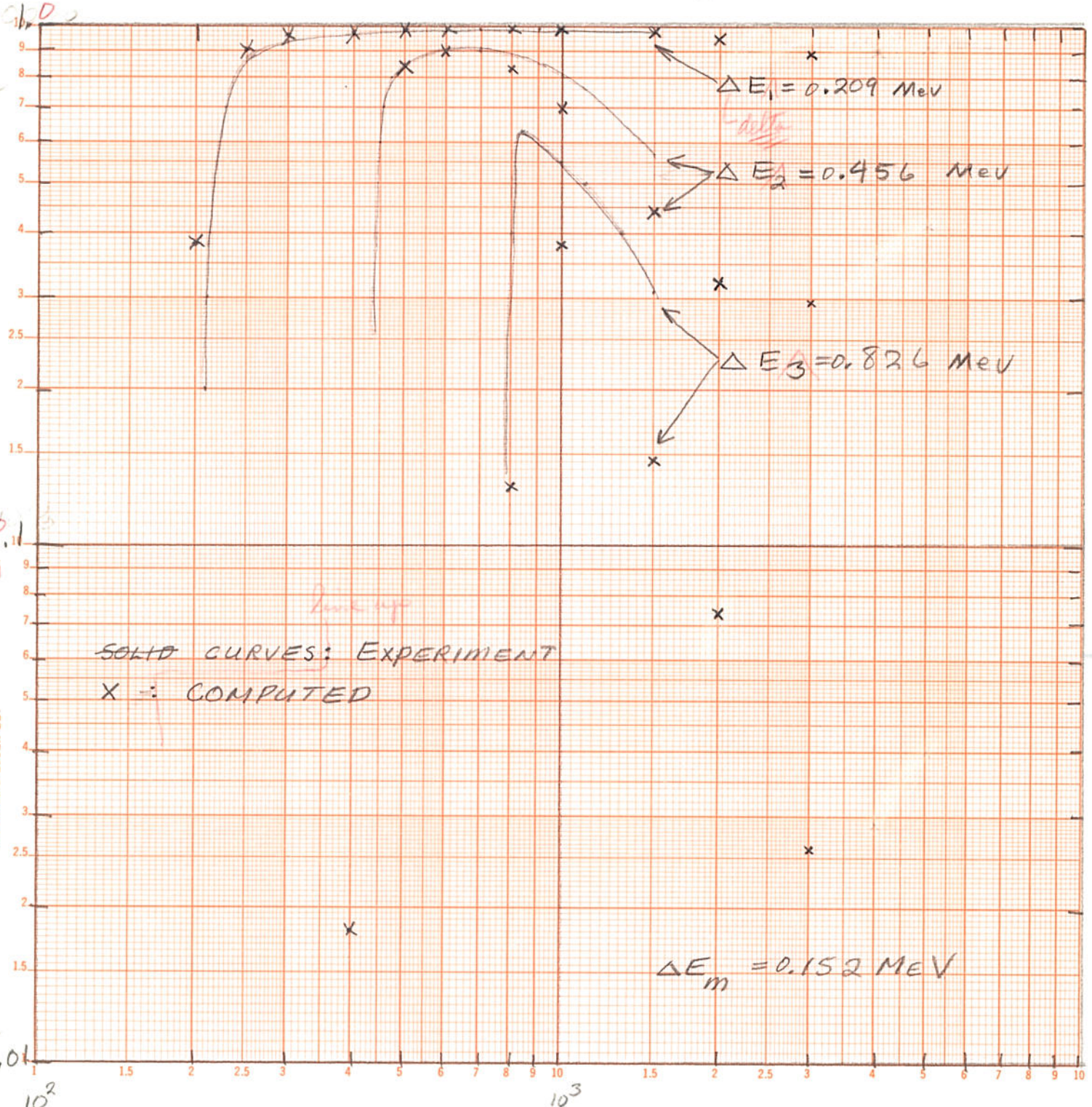
rec 10/12

due 10/19

COMPARISON OF COMPUTED AND EXPERIMENTAL RELATIVE ELECTRON EFFICIENCIES

KHI 10 CHANNEL COUNTING

K&E LOGARITHMIC 46 7203 MADE IN U.S.A. KEUFFEL & ESSER CO.



Energy (keV)

FIGURE 1

70%