

FIGURE IX-1

IX-67

Approved

P.E. Carlson

Date

Mo. 10, 1971

$$T = \frac{10 \log \left(\frac{V+1.0}{3.21} \right)}{\log \left(\frac{2.728}{3.21} \right)} = \frac{10 \log \left(\frac{V+1.0}{3.21} \right)}{\log (0.850)}$$

$$\log 0.850 = 0.9294 - 1.0 = 0.0706 \\ = -0.706$$

$$T = \frac{10}{(-0.706)} \log \left(\frac{V+1.0}{3.21} \right)$$

$$T = -14.16 \log \left(\frac{V+1.0}{3.21} \right) {}^{\circ}\text{C}$$

$$\text{sample point } T=30 \quad V=0.973$$

$$T = -141.6 \underbrace{\log \left(\frac{1.973}{3.21} \right)}_{\begin{array}{c} \cdot 6146 \\ - .2111 \end{array}} = 29.9 {}^{\circ}$$

$$T=40 \quad V=.715$$

$$T = -141.6 \underbrace{\log \left(\frac{1.715}{3.21} \right)}_{\cdot 2725} = 38.6 {}^{\circ}$$

$$T = 50^\circ \quad V = 1.52$$

$$T = -141.6 \log \underbrace{\frac{1.52}{3.21}}_{-0.3242} = 45.9^\circ$$

$$T = -10^\circ \quad V = 2.71 \quad = -8.86^\circ$$

$$T = -141.6 \log \underbrace{\frac{3.71}{3.21}}_{0.1156} \underbrace{\frac{1.156}{0.626}}_{-0.626}$$

$$T = -20^\circ \quad V = 3.183 \quad = -16.28$$

$$T = -141.6 \log \underbrace{\frac{4.183}{3.21}}_{1.303}$$

$$T = -30^\circ \quad T = -141.6 \log \frac{4.57}{3.21} = -21.7$$

$$T = +20 \quad T = -141.6 \log \frac{2.267}{3.21} = 21.5$$

$$T = +10 \quad T = -141.6 \log \frac{2.728}{3.21} = 10.0$$

T_{exp}	$T_{calc}^{(1)}$	Δ $T_{calc} - T_{exp}$	V	$-0.656(V-1.728)^3$
-30	-21.7	+8.3	.52.	+11.56
-20	-16.3	+3.7	.715	
-10	-8.9	+1.1	.973	
0	0	0	1.267	
10	10.0	0	1.728	
20	21.5	1.5	2.21	
30	29.9	0	2.71	
40	38.6	-1.4	3.183	
50	45.9	-4.1	3.57	

$$conv = A (V - 1.728)^3 =$$

$$A (3.57 - 1.728)^3 = -4.1$$

$$A = \frac{-4.1}{(3.57 - 1.728)^3} = \frac{-4.1}{6.251} = -0.656$$

$$\log(V+1.0) = AT + B$$

50 .52

$$T=0$$

$$B = \log 3.21$$

.195

40 .715

$$0.063$$

$$AT = \log(V+1.0) - \log 3.21$$

.258

30 .973

$$0.036$$

$$T = \frac{1}{A} \log\left(\frac{V+1.0}{3.21}\right)$$

.294

20 1.267

$$0.167$$

.461

10 1.728

$$0.021$$

.482

0 2.21

$$0.018$$

.508

-10 2.71

$$-0.027$$

.473

-20 3.183

$$-0.086$$

.387

-30 3.57

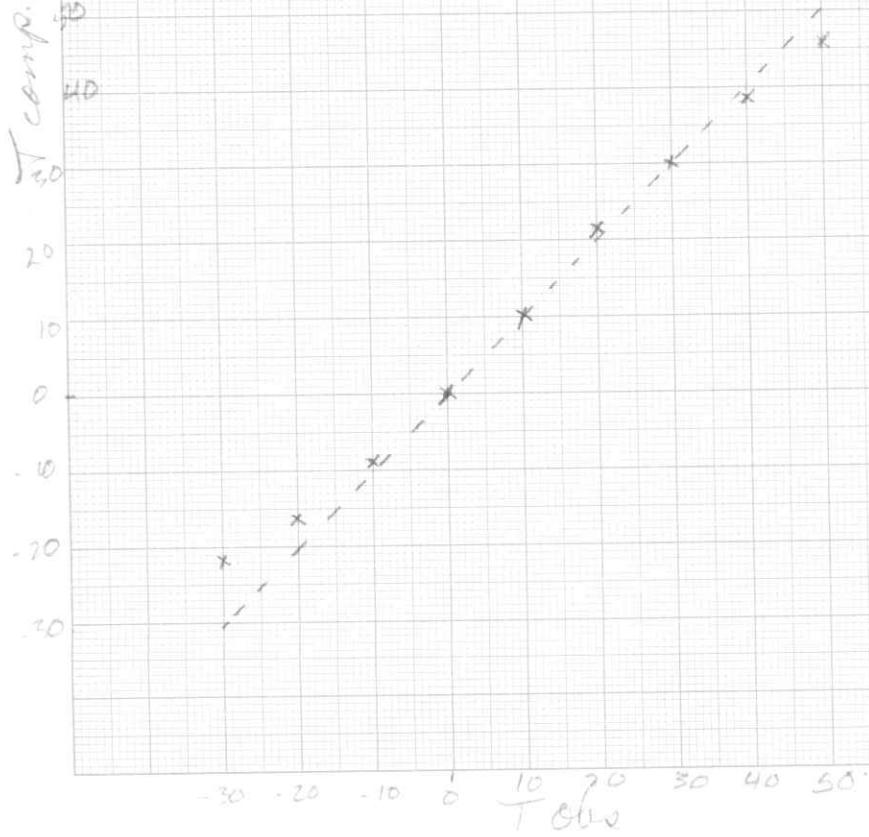
$$T = \frac{1}{A} \log\left(\frac{V+1.0}{3.21}\right)$$

$$A = \frac{T}{\log\left(\frac{V+1.0}{3.21}\right)}$$

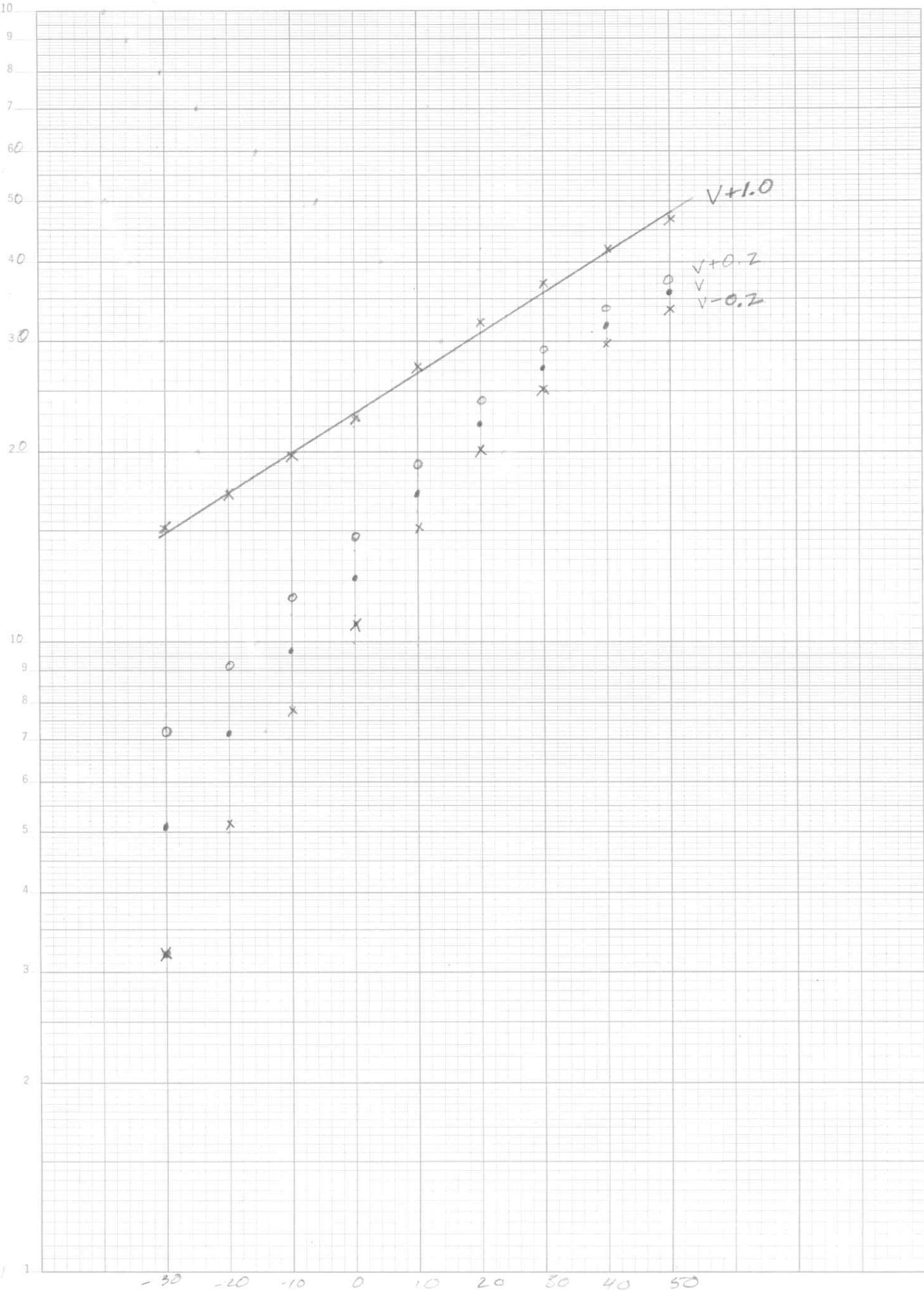
$$A = \frac{10}{\log\left(\frac{2.728}{3.21}\right)}$$

$$A = \frac{1}{10} \log\left(\frac{2.728}{3.21}\right)$$

K_g 10 X 10 TO THE CENTIMETER 46 1513
10 X 25 CM. 1.0 IN U.S.A.
KEUFFEL & ESSER CO.



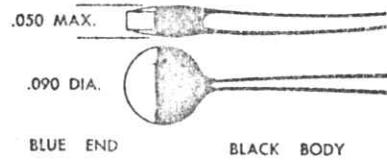
SEMI LOGARITHMIC
KEUFFEL & ESSER CO., NEW YORK,
2 CYCLES X 70 DIVISIONS



YSI PRECISE THERMISTOR

10,000 OHMS AT 25°C

PART No. 44006



#32 TINNED
COPPER WIRE
3" LONG

TIME CONSTANT:*

1 second maximum. This value was determined with the thermistor suspended by its leads in a "well stirred" oil bath.

10 seconds maximum. This value was determined with the thermistor suspended by its leads in still air.

*Time constant is the time required for the thermistor to indicate 63% of a new impressed temperature.

DISSIPATION CONSTANT:**

8 mw/°C. This value was determined with the thermistor suspended by its leads in a "well stirred" oil bath.

1 mw/°C. This value was determined with the thermistor suspended by its leads in still air.

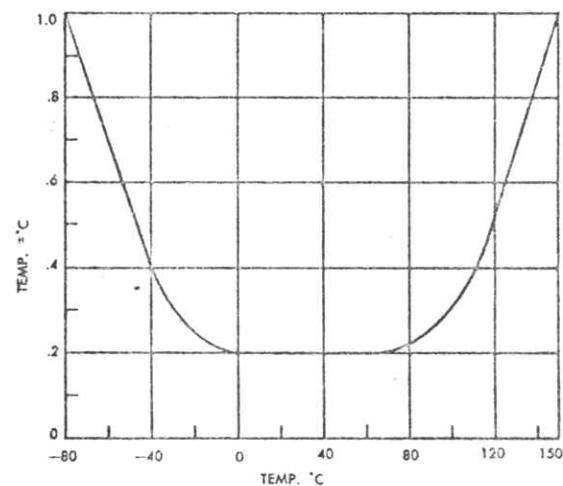
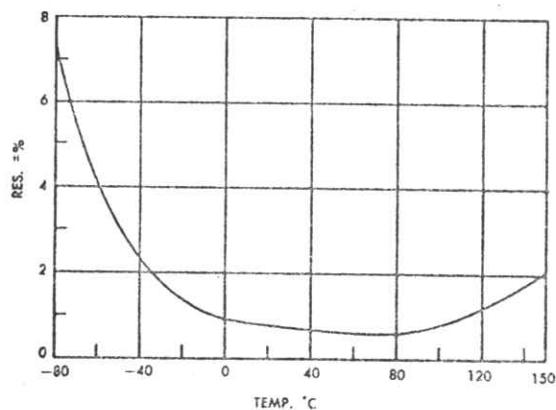
**The dissipation constant is the amount of power in milliwatts required to raise the thermistor 1°C above the surrounding temperature.

COLOR CODE:

Black epoxy on the body of the thermistor with blue end. Maximum operating temperature 150°C.

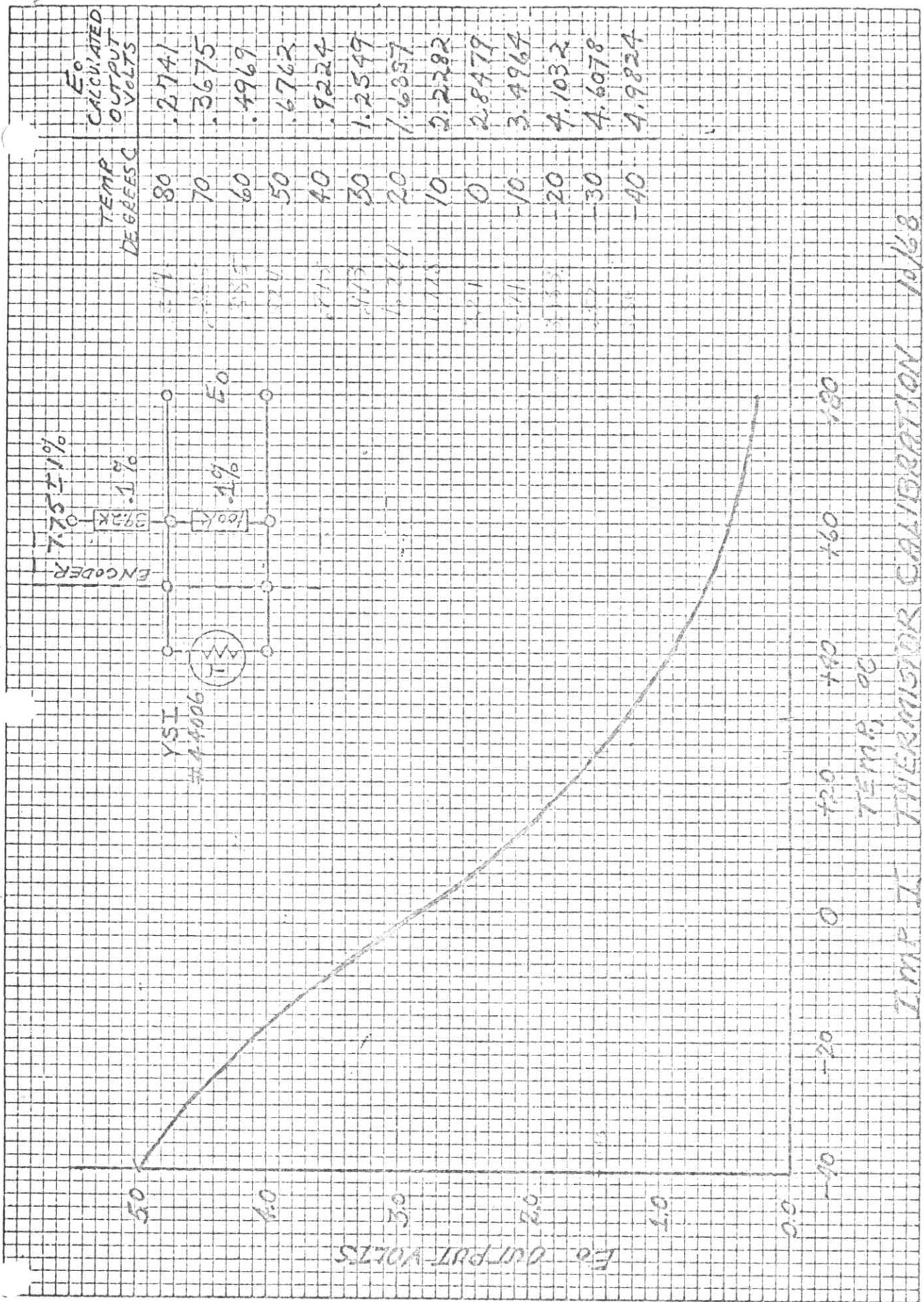
TOLERANCES

Preliminary Data, Sept. 15, 1961



RESISTANCE VERSUS TEMPERATURE - 60°C to +150°C

TEMP. °C	RES.Ω	TEMP. °C	RES.Ω	TEMP. °C	RES.Ω	TEMP. °C	RES.Ω	TEMP. °C	RES.Ω	TEMP. °C	RES.Ω	TEMP. °C	RES.Ω
-80	355K	-41	304.6K	-8	43.11K	28	8867	61	2417	100	816.8	136	326.3
79	329K	43	286.7K	7	11.07K	29	8523	65	2337	101	794.6	137	313.7
78	305K	42	270.0K	6	39.11K	30	8194	66	2244	102	773.1	138	311.3
77	283K	41	254.1K	5	37.31K	31	7880	67	2191	103	752.3	139	297.2
76	262K	40	239.3K	4	35.57K	32	7579	68	2152	104	732.1	140	287.1
75	244K	39	226.0K	3	33.93K	33	7291	69	1955	105	712.6	111	275.1
74	226K	38	213.2K	2	32.37K	34	7016	70	1990	106	693.6	112	263.0
73	210K	37	201.1K	1	30.89K	35	6752	71	1928	107	675.3	113	257.0
72	195K	36	189.8K	0	29.41K	36	6500	72	1888	108	657.5	114	247.1
71	182K	35	179.2K	1	28.05K	37	6258	73	1810	109	640.3	115	237.1
70	169K	34	169.3K	2	26.89K	38	6026	74	1755	110	623.5	116	229.2
69	157K	33	160.0K	3	25.65K	39	5805	75	1700	111	607.3	117	223.1
68	146K	32	151.2K	4	24.45K	40	5572	76	1618	112	591.6	118	217.5
67	135K	31	143.0K	5	23.34K	41	5389	77	1559	113	576.4	119	212.3
66	127K	30	135.2K	6	22.34K	42	5193	78	1509	114	561.6	120	207.0
65	119K	29	127.5K	7	21.45K	43	5006	79	1503	115	547.3	121	201.2
64	111K	28	121.1K	8	20.65K	44	4827	80	1458	116	533.4	122	195.1
63	103K	27	114.6K	9	19.63K	45	4655	81	1414	117	519.9	123	189.6
62	96K	26	108.6K	10	18.75K	46	4479	82	1372	118	506.8	124	184.2
61	90.1K	25	102.9K	11	17.95K	47	4331	83	1332	119	491.1	125	178.5
60	84.5K	24	97.1K	12	17.22K	48	4179	84	1293	120	481.8	126	173.0
59	79.1K	23	92.4K	13	16.46K	49	4033	85	1255	121	469.8	127	167.4
58	74.0K	22	87.6K	14	15.75K	50	3873	86	1218	122	458.2	128	161.8
57	69.2K	21	83.1K	15	15.13K	51	3758	87	1183	123	446.9	129	156.2
56	65.3K	20	78.9K	16	14.50K	52	3639	88	1150	124	435.9	130	150.7
55	62.7K	19	74.9K	17	13.90K	53	3526	89	1116	125	425.3	131	145.2
54	59.6K	18	71.1K	18	13.33K	54	3305	90	1084	126	141.9	132	139.7
53	56.4K	17	67.5K	19	12.79K	55	3170	91	1053	127	136.9	133	134.1
52	53.1K	15	64.2K	20	12.26K	56	3160	92	1023	128	135.1	134	128.5
51	50.1K	15	61.0K	21	11.77K	57	3054	93	994.2	129	135.6	135	123.6
50	47.1K	14	58.0K	22	11.29K	58	2952	94	966.3	130	136.4	136	118.4
49	44.1K	13	55.1K	23	10.80K	59	2854	95	939.3	131	137.4	137	113.4
48	41.1K	12	52.6K	24	10.41K	60	2760	96	913.2	132	138.7	138	108.7
47	38.6K	11	49.9K	25	10.00K	61	2669	97	887.9	133	139.3	139	104.3
46	36.1K	10	47.5K	26	9.605	62	2562	98	863.4	134	132.0	140	99.0
45	33.7K	-9	45.27K	27	9.227	63	2467	99	839.7	135	334.0		



THE JOHNS HOPKINS UNIVERSITY

APPLIED PHYSICS LABORATORY

8621 GEORGIA AVENUE

SILVER SPRING, MARYLAND 20910

TELEPHONE
776-7100
589-7700
AREA CODE 301

MAR 19 1970

Please refer to:
TSSD-1847

Director
National Aeronautics and Space Administration
Goddard Space Flight Center
Greenbelt, Maryland 20771

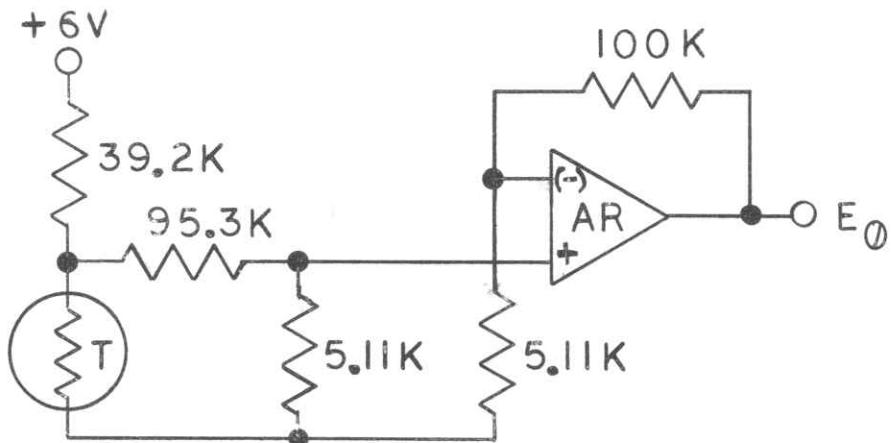
Attention: Mr. William R. Limberis, Code 724

Subject: Temperature Monitor on APP Experiment, IMP H and J
(APL, Dr. S. M. Krimigis).

Dear Sir:

This letter is in response to your request for information on the APL method of measuring the APP package temperature. One such measurement will be made by a thermistor mounted on the Proton Electron Telescope. This output is sub-commutated onto the analog performance parameter as one of eight (8) measurements. The thermistor to be used is a YSI 44006 furnished by the project office. We will require a total of four (4) units, three (3) to be used in the flight units plus one spare. We require at least one such thermistor by May 1, 1970 in order to meet our production schedule for the protoflight package.

APL will use the same network used by GSFC for making temperature measurements. However, the supply voltage is different from that used by GSFC (6.0V vs. 7.75V) and there are gain changes in the sub-commutation process. The circuit is shown below in a simplified form.



This schematic shows that the thermistor voltage is attenuated by a factor of 20 and then multiplied by a factor of 20 in an operational amplifier. The net effect is that the calibration curve is the same as that given by the project office multiplied by a factor of 0.775 (6.0V/7.75V).

If any additional information is desired about the temperature monitor, please contact R. E. Cashion at telephone number 776-7100, extension 2068.

Very truly yours,

R. B. Kershner
Space Development
Department Head

REC
RBK:REC:ks

Distribution:

NAVPLANTREPO/SS
NAVAIRSYSCOM/Code AIR-538

Dr. J. Trainer, GSFC, Code 611
Dr. N. Ness, GSFC, Code 616
Mr. B. Ferer, GSFC, Code 724
Mr. D. Lokerson, GSFC, Code 711
Dr. T. Armstrong, Univ. of Kansas